



Australian Government  
Department of Defence  
Defence Science and  
Technology Organisation



THE UNIVERSITY  
OF ADELAIDE  
AUSTRALIA

# Polarimetric Calibration of the *Ingara* Bistatic SAR

Alvin Goh,<sup>1,2</sup> Mark Preiss,<sup>1</sup> Nick Stacy,<sup>1</sup> Doug Gray<sup>2</sup>

1. Imaging Radar Systems Group  
Defence Science and Technology Organisation

2. School of Electrical & Electronic Engineering  
University of Adelaide



Australian Government  
 Department of Defence  
 Defence Science and  
 Technology Organisation



# Bistatic SAR experiments

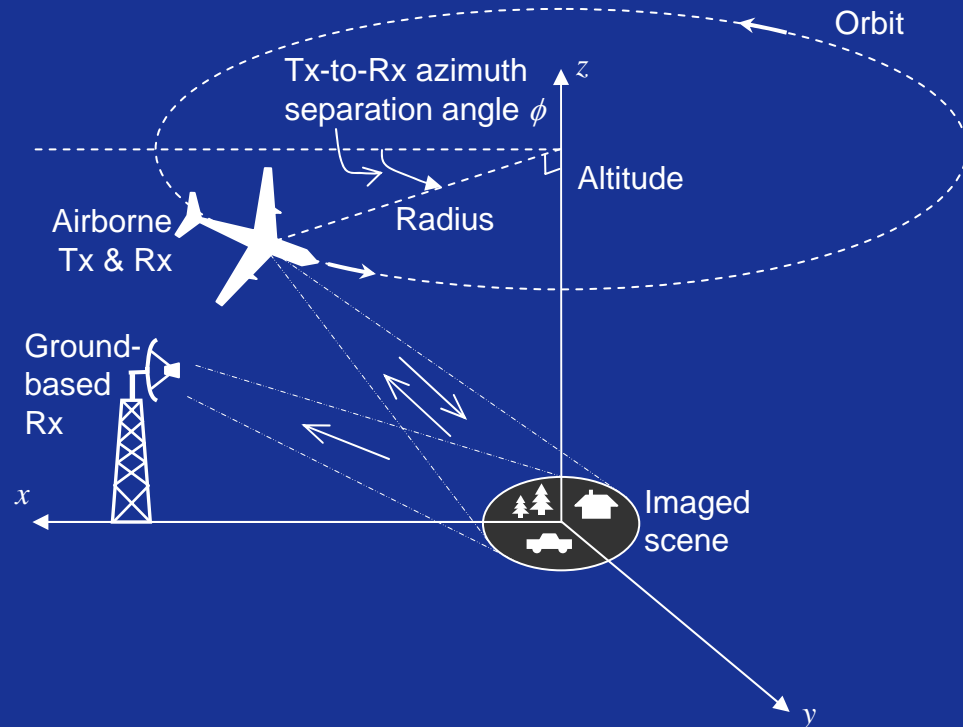
Reciprocity  $\Rightarrow s_{hv} = s_{vh}$  in monostatic but not bistatic: potentially more information in bistatic measurements

Supplement *Ingara* X-band full-pol. airborne SAR with stationary full-pol. ground-based receiver on 15 metre high tower

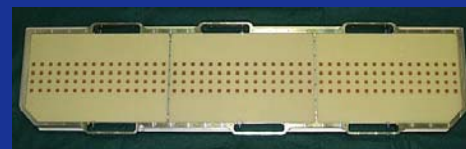
Synch. using GPS 1PPS; operate at fixed 650 Hz PRF

Operate in circular spotlight-SAR mode:  
 orbit radii 3 – 6 km; altitudes 1000 – 3600 m;  
 incidence angles  $53^\circ - 82^\circ$

Simultaneously collect 600 MHz bandwidth full-pol. monostatic and bistatic data over wide variety of angles



Beechcraft 1900C



Airborne Tx & Rx antenna



Ground-based Rx-only antenna



# Polarimetric measurement model

Polarimetric measurement model is

$$\mathbf{O} = \mathbf{R} \mathbf{S} \mathbf{T} + \mathbf{N}$$

in which

$$\mathbf{O} = \begin{bmatrix} o_{hh} & o_{hv} \\ o_{vh} & o_{vv} \end{bmatrix}$$

*Measurements*

$$\mathbf{R} = \begin{bmatrix} r_{hh} & r_{hv} \\ r_{vh} & r_{vv} \end{bmatrix}$$

*Receive distortion*

$$\mathbf{S} = \begin{bmatrix} s_{hh} & s_{hv} \\ s_{vh} & s_{vv} \end{bmatrix}$$

*Target scattering*

$$\mathbf{T} = \begin{bmatrix} t_{hh} & t_{hv} \\ t_{vh} & t_{vv} \end{bmatrix}$$

*Transmit distortion*

$$\mathbf{N} = \begin{bmatrix} n_{hh} & n_{hv} \\ n_{vh} & n_{vv} \end{bmatrix}$$

*Noise*

By rewriting  $\mathbf{O}$ ,  $\mathbf{S}$ ,  $\mathbf{N}$  as  $\mathbf{o} = (o_{hh}, o_{hv}, o_{vh}, o_{vv})^T$ ,  $\mathbf{s} = (s_{hh}, s_{hv}, s_{vh}, s_{vv})^T$ ,  $\mathbf{n} = (n_{hh}, n_{hv}, n_{vh}, n_{vv})^T$ , we obtain

$$\mathbf{o} = \mathbf{P} \mathbf{s} + \mathbf{n}$$

where

$$\mathbf{P} = \mathbf{Y} \mathbf{M} \mathbf{A} \mathbf{K}$$

$$\mathbf{M} = \begin{bmatrix} 1 & v & w & vw \\ z & 1 & wz & w \\ u & uv & 1 & v \\ uz & u & z & 1 \end{bmatrix}$$

$$\mathbf{A} = \begin{bmatrix} \alpha & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & \alpha & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

$$\mathbf{K} = \begin{bmatrix} k^2 & 0 & 0 & 0 \\ 0 & k & 0 & 0 \\ 0 & 0 & k & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

in which

$$\underbrace{Y = r_{vv} t_{vv}}_{\text{Absolute scaling factor}}$$

$$\underbrace{k = r_{hh}/r_{vv} \quad \alpha = t_{hh}r_{vv}/t_{vv}r_{hh}}_{\text{Channel-imbalance parameters}}$$

$$\underbrace{u = r_{vh}/r_{hh}, v = t_{vh}/t_{vv}, w = r_{hv}/r_{vv}, z = t_{hv}/t_{hh}}_{\text{Cross-talk ratios}}$$

Polarimetric calibration involves estimation of  $k$ ,  $\alpha$ ,  $u$ ,  $v$ ,  $w$ ,  $z$  (leaving  $Y$  to radiometric calibration).



# Distributed-target methods 1

For a distributed-target, can calculate covariance matrices

$$\mathbf{C}_o = \begin{bmatrix} \langle |o_{hh}|^2 \rangle & \langle o_{hh} o_{hv}^* \rangle & \langle o_{hh} o_{vh}^* \rangle & \langle o_{hh} o_{vv}^* \rangle \\ \langle o_{hv} o_{hh}^* \rangle & \langle |o_{hv}|^2 \rangle & \langle o_{hv} o_{vh}^* \rangle & \langle o_{hv} o_{vv}^* \rangle \\ \langle o_{vh} o_{hh}^* \rangle & \langle o_{vh} o_{hv}^* \rangle & \langle |o_{vh}|^2 \rangle & \langle o_{vh} o_{vv}^* \rangle \\ \langle o_{vv} o_{hh}^* \rangle & \langle o_{vv} o_{hv}^* \rangle & \langle o_{vv} o_{vh}^* \rangle & \langle |o_{vv}|^2 \rangle \end{bmatrix} \quad \mathbf{C}_s = \begin{bmatrix} \langle |s_{hh}|^2 \rangle & \langle s_{hh} s_{hv}^* \rangle & \langle s_{hh} s_{vh}^* \rangle & \langle s_{hh} s_{vv}^* \rangle \\ \langle s_{hv} s_{hh}^* \rangle & \langle |s_{hv}|^2 \rangle & \langle s_{hv} s_{vh}^* \rangle & \langle s_{hv} s_{vv}^* \rangle \\ \langle s_{vh} s_{hh}^* \rangle & \langle s_{vh} s_{hv}^* \rangle & \langle |s_{vh}|^2 \rangle & \langle s_{vh} s_{vv}^* \rangle \\ \langle s_{vv} s_{hh}^* \rangle & \langle s_{vv} s_{hv}^* \rangle & \langle s_{vv} s_{vh}^* \rangle & \langle |s_{vv}|^2 \rangle \end{bmatrix} \quad \mathbf{C}_n = \begin{bmatrix} \langle |n_{hh}|^2 \rangle & \langle n_{hh} n_{hv}^* \rangle & \langle n_{hh} n_{vh}^* \rangle & \langle n_{hh} n_{vv}^* \rangle \\ \langle n_{hv} n_{hh}^* \rangle & \langle |n_{hv}|^2 \rangle & \langle n_{hv} n_{vh}^* \rangle & \langle n_{hv} n_{vv}^* \rangle \\ \langle n_{vh} n_{hh}^* \rangle & \langle n_{vh} n_{hv}^* \rangle & \langle |n_{vh}|^2 \rangle & \langle n_{vh} n_{vv}^* \rangle \\ \langle n_{vv} n_{hh}^* \rangle & \langle n_{vv} n_{hv}^* \rangle & \langle n_{vv} n_{vh}^* \rangle & \langle |n_{vv}|^2 \rangle \end{bmatrix}$$

whereupon

$$\mathbf{C} = \mathbf{C}_o - \mathbf{C}_n = \mathbf{P} \mathbf{C}_s \mathbf{P}^H$$

Covariance matrix of distributed-target is commonly postulated to have the simple form:

$$\mathbf{C}_s = \begin{bmatrix} \sigma_{11} & 0 & 0 & \sigma_{41}^* \\ 0 & \beta & \beta & 0 \\ 0 & \beta & \beta & 0 \\ \sigma_{41} & 0 & 0 & \sigma_{44} \end{bmatrix} \quad \text{from} \quad \begin{cases} s_{hv} = s_{vh} \text{ (scattering reciprocity)} \\ \langle s_{ii} s_{jj} \rangle = \langle s_{jj} s_{ii} \rangle = 0 \text{ (azimuthal symmetry)} \end{cases}$$

This provides the basis for calculating  $\alpha$ ,  $u$ ,  $v$ ,  $w$ ,  $z$  from an input covariance matrix  $\mathbf{C}$ :

Ainsworth TL, Ferro-Famil L, Lee J-S, 2006, "Orientation angle preserving *a posteriori* polarimetric SAR calibration," *IEEE Trans. Geosci. Remote Sens.*, **44**(4): 994-1003.

Klein JD, 1992, "Calibration of complex polarimetric SAR imagery using backscatter correlations," *IEEE Trans. Aerosp. Electron. Syst.*, **28**(1): 183-94.

Lopez-Martinez C, Cortes A, Fabregas X, 2007, "Analysis and improvement of polarimetric calibration techniques," *Proc. IGARSS 2007*, Barcelona, Spain, p. 5224-7.

Quegan S, 1994, "A unified algorithm for phase and cross-talk calibration of polarimetric data - theory and observations," *IEEE Trans. Geosci. Remote Sens.*, **32**(1): 89-99.



Australian Government  
 Department of Defence  
 Defence Science and  
 Technology Organisation



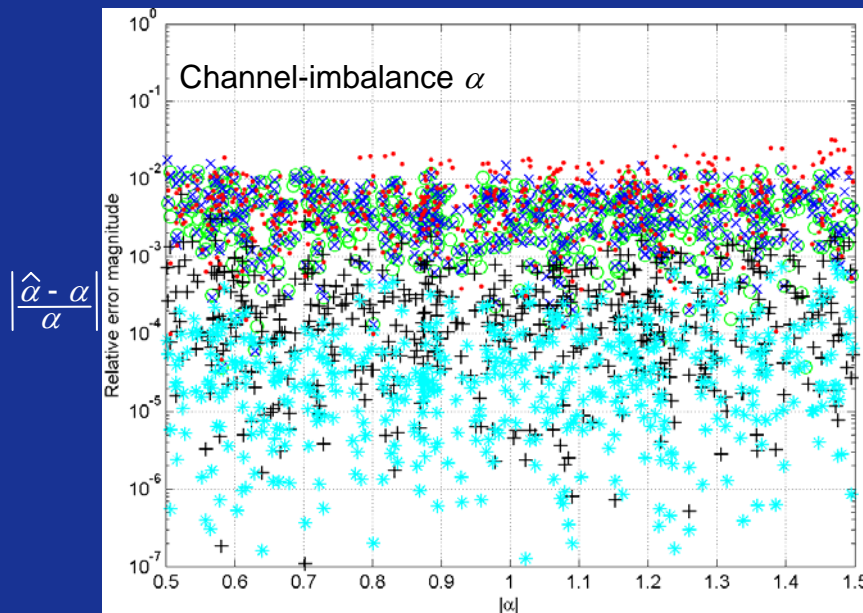
# Distributed-target methods 2

Examine a variety of methods:

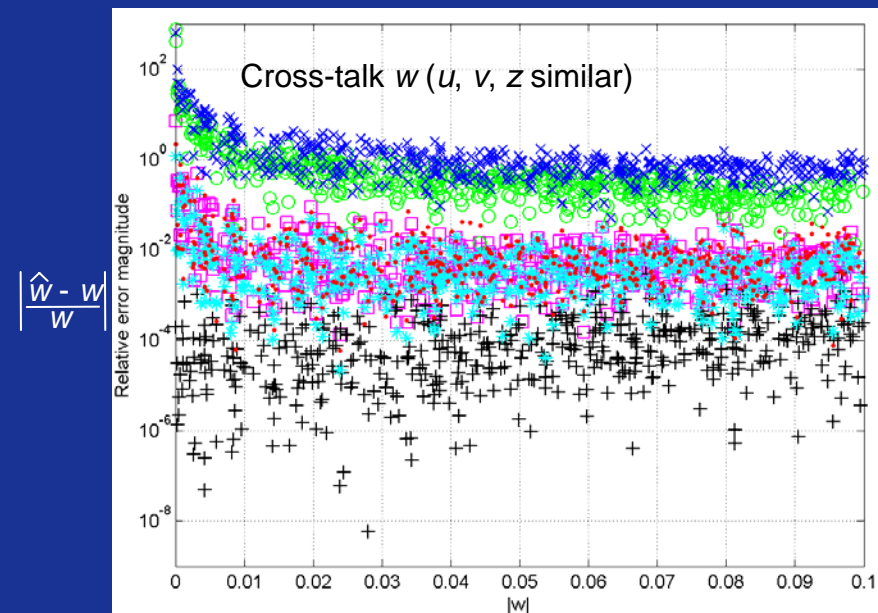
- $K$ : use eigenvector of  $\mathbf{C}$  (Klein 1992)
- $Q$ : use linear-approximations to  $\mathbf{C}$  (Quegan 1994)
- ×  $A$ : transform  $\mathbf{C}$  into postulated  $\mathbf{C}_s$  form while accommodating non-zero azimuthal slope (Ainsworth *et al.* 2006)
- \*  $Ka$ :  $K$  with improved estimation of  $\alpha$
- $Qi$ :  $Q$  with iterations (Lopez-Martinez *et al.* 2007)
- +  $Az$ :  $A$  with enforced azimuthal symmetry

Compare accuracy using numerical simulations:  $\left\{ \begin{array}{l} \text{Set } \sigma_{11} = \sigma_{44} = 0 \text{ dB, } |\sigma_{41}| = -1 \text{ dB, } \beta = -12 \text{ dB, } Y = k = 1 \\ \text{Randomly assign } 0 < |u|, |v|, |w|, |z| < 0.1, 0.5 < |\alpha| < 1.5, \\ 0 \leq \angle\sigma_{41}, \angle\alpha, \angle u, \angle v, \angle w, \angle z < 2\pi \end{array} \right.$

Results with full noise-compensation, i.e.  $\mathbf{C} = \mathbf{C}_o - \mathbf{C}_n$



$Ka$  has lowest  $\alpha$ -estimation error



$Az$  has lowest cross-talk estimation error



# Calibration-target methods

Model for calibration target measurements when cross-talk is negligible (or already corrected) is

$$\begin{aligned} o_{hh} &= Y k^2 \alpha s_{hh} \\ o_{hv} &= Y k s_{hv} \\ o_{vh} &= Y k \alpha s_{vh} \\ o_{vv} &= Y s_{vv} \end{aligned} \quad (\text{noise assumed negligible})$$

Hence, from measurements of a depolarising target with known  $s_{vh}/s_{hv}$ , we can estimate  $\alpha$  via

$$\alpha = \frac{o_{vh}/o_{hv}}{s_{vh}/s_{hv}}$$

With a previously-obtained estimate of  $\alpha$ , and measurements of a target with known  $s_{hh}/s_{vv}$ , we can estimate  $\pm k$  via

$$k = \pm \sqrt{\frac{o_{hh}/o_{vv}}{\alpha s_{hh}/s_{vv}}} \quad (1)$$

From measurements of a depolarising target with known  $s_{hh}/s_{vh}$  or  $s_{hv}/s_{vv}$ , we can also estimate  $k$  via

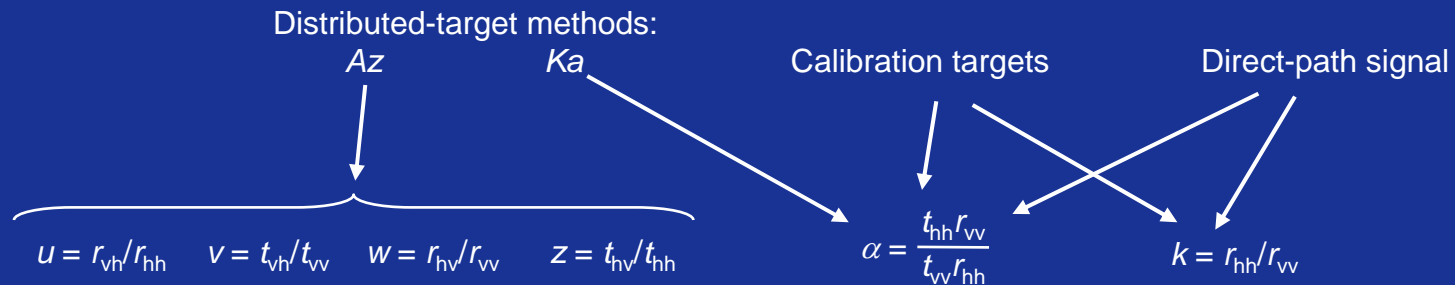
$$k = \frac{o_{hh}/o_{vh}}{s_{hh}/s_{vh}} \quad k = \frac{o_{hv}/o_{vv}}{s_{hv}/s_{vv}} \quad (2)$$

We can also just use (2) to resolve the sign ambiguity in (1).

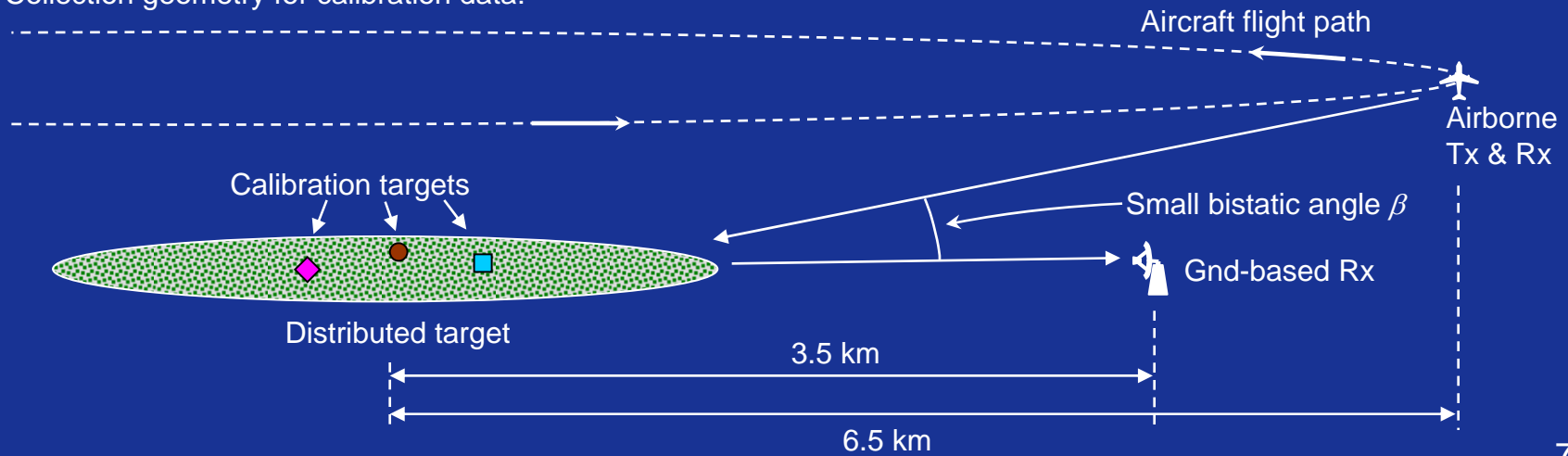
For bistatic system, direct-path signal can also be used in lieu of calibration target.



# Polarimetric calibration



Collection geometry for calibration data:

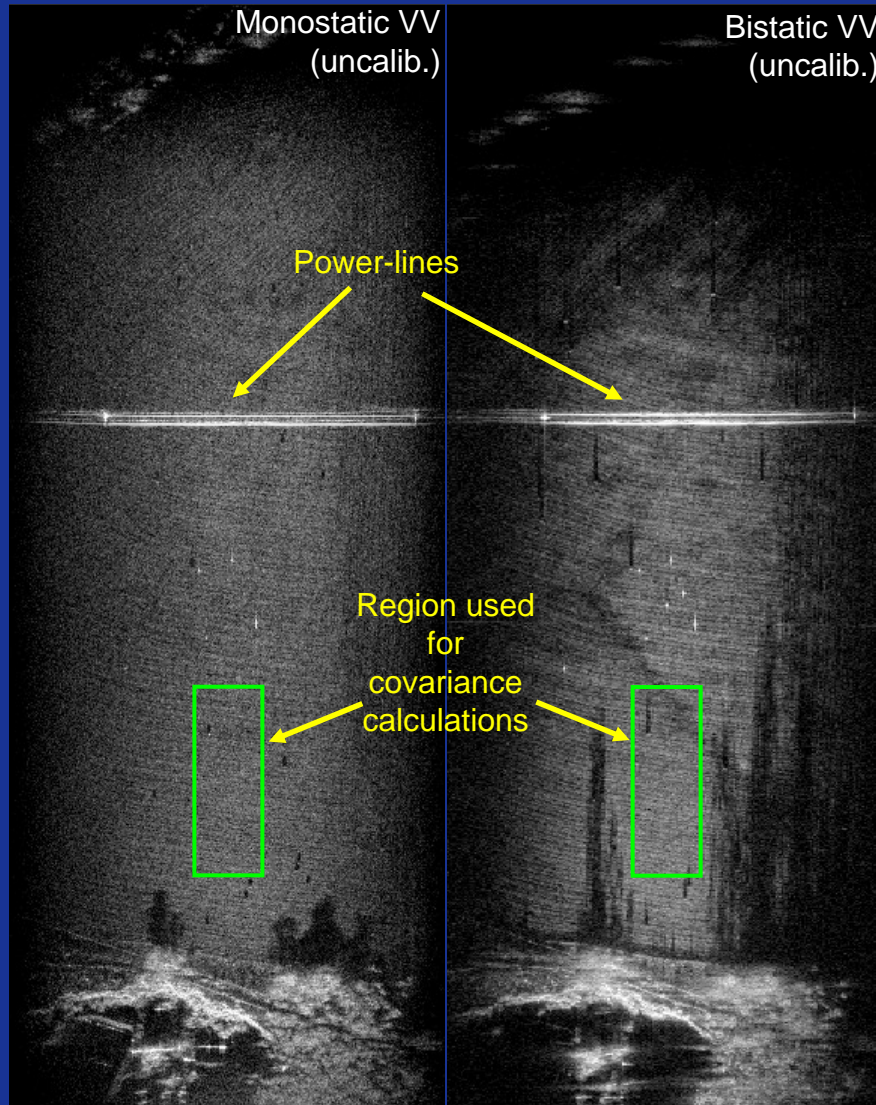




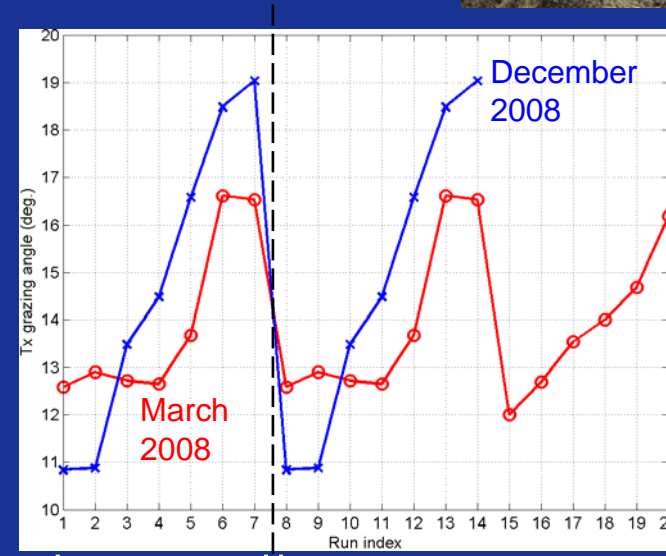
Australian Government  
 Department of Defence  
 Defence Science and  
 Technology Organisation



# Distributed-target measurements 1



March 2008 images



Runs 1-7:  
Airborne Rx  
(monostatic)

Runs 8-20:  
Ground-based Rx  
(bistatic)

Grazing angle of ground-based Rx  $\approx 2^\circ$

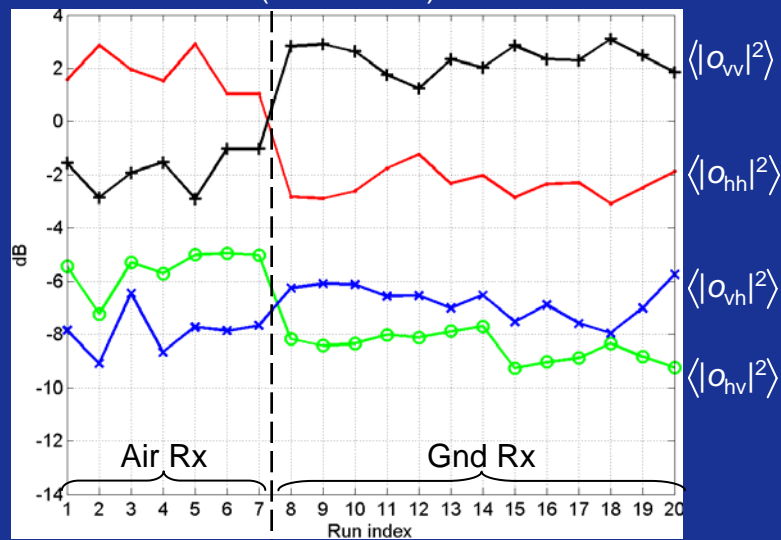




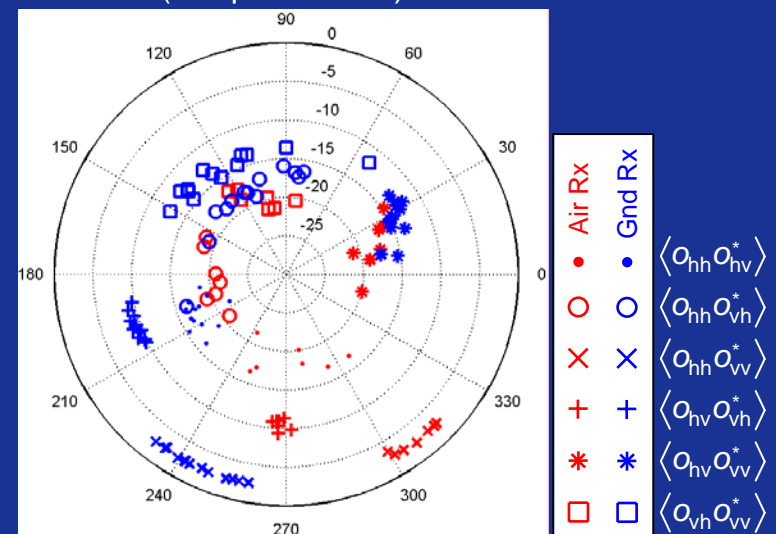
# Distributed-target measurements 2

Measured covariance matrix  $\mathbf{C}_o = \begin{bmatrix} \langle |o_{hh}|^2 \rangle & \langle o_{hh} o_{hv}^* \rangle & \langle o_{hh} o_{vh}^* \rangle & \langle o_{hh} o_{vv}^* \rangle \\ \langle o_{hv} o_{hh}^* \rangle & \langle |o_{hv}|^2 \rangle & \langle o_{hv} o_{vh}^* \rangle & \langle o_{hv} o_{vv}^* \rangle \\ \langle o_{vh} o_{hh}^* \rangle & \langle o_{vh} o_{hv}^* \rangle & \langle |o_{vh}|^2 \rangle & \langle o_{vh} o_{vv}^* \rangle \\ \langle o_{vv} o_{hh}^* \rangle & \langle o_{vv} o_{hv}^* \rangle & \langle o_{vv} o_{vh}^* \rangle & \langle |o_{vv}|^2 \rangle \end{bmatrix}$

On-diagonal covariances  
 (real-valued)



Off-diagonal covariances  
 (complex-valued)



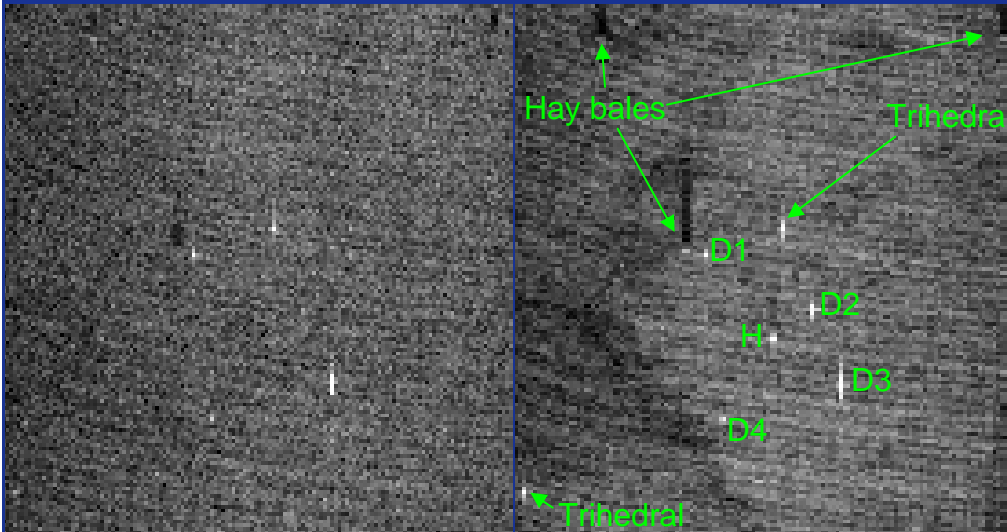


Australian Government  
 Department of Defence  
 Defence Science and  
 Technology Organisation  
 Air Rx (monostatic)



# Calibration target measurements 1

Gnd Rx (bistatic)



March 2008 SAR images

Hemisphere  $k = \pm \sqrt{\frac{\sigma_{hh}}{\alpha \sigma_{vv}}}$

Upright dihedral  $k = \pm j \sqrt{\frac{\sigma_{hh}}{\alpha \sigma_{vv}}}$

Tilted dihedral  $\begin{cases} \alpha = \sigma_{vh}/\sigma_{hv} \\ k = \pm j \sqrt{\frac{\sigma_{hh}}{\alpha \sigma_{vv}}} = \frac{\sigma_{hh}}{\sigma_{vh}} \tan 2\varphi = -\frac{\sigma_{hv}}{\sigma_{vv}} \cot 2\varphi \end{cases}$

Tilt  $\varphi = -22.5^\circ$

D1: tilted 25 cm dihedral  
 $S = \begin{bmatrix} 1 & -1 \\ -1 & -1 \end{bmatrix}$



D2: upright 25 cm dihedral  
 $S = \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix}$



H:  $\varnothing 112$  cm hemisphere  
 $S = \begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix}$

Tilt  $\varphi = +22.5^\circ$

D4: tilted 54 cm dihedral  
 $S = \begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix}$

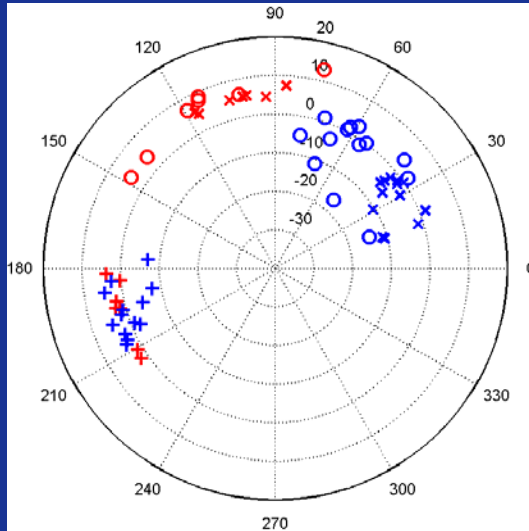


D3: upright 54 cm dihedral  
 $S = \begin{bmatrix} 1 & 0 \\ 0 & -1 \end{bmatrix}$





# Calibration target measurements 2

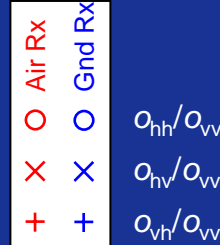


D1:

$$S_{hh}/S_{vv} = -1$$

$$S_{hv}/S_{vv} = +1$$

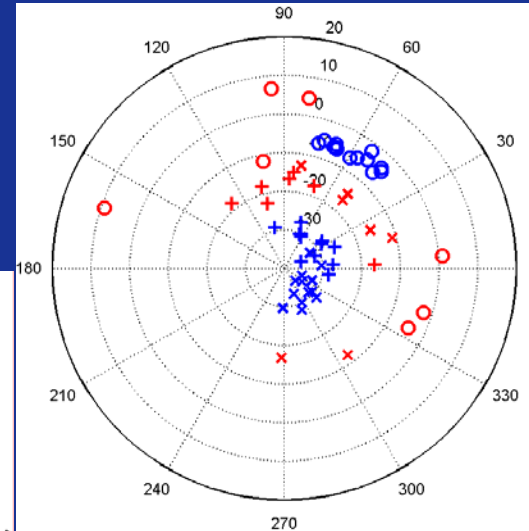
$$S_{vh}/S_{vv} = +1$$



$$O_{hh}/O_{vv}$$

$$O_{hv}/O_{vv}$$

$$O_{vh}/O_{vv}$$

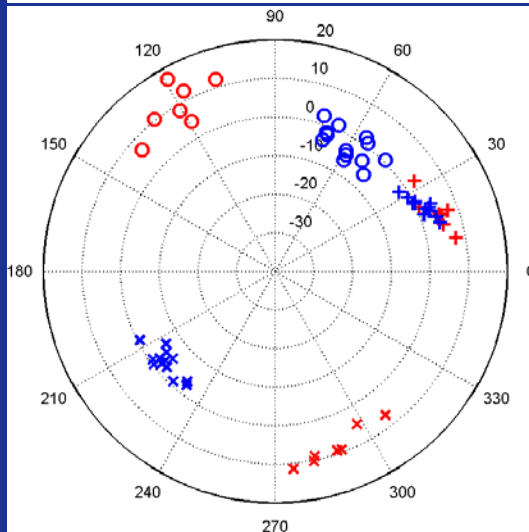


D2:

$$S_{hh}/S_{vv} = -1$$

$$S_{hv}/S_{vv} = 0$$

$$S_{vh}/S_{vv} = 0$$

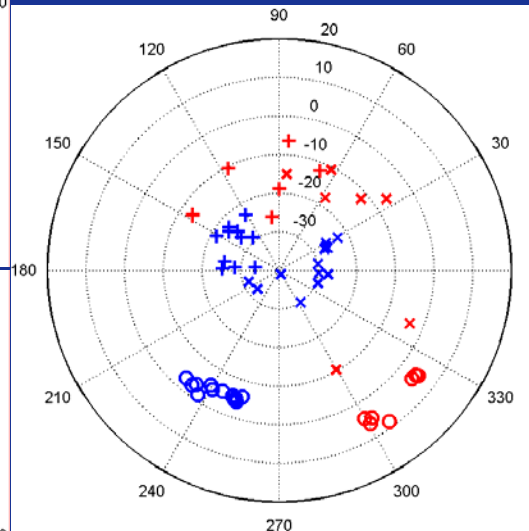


D3:

$$S_{hh}/S_{vv} = -1$$

$$S_{hv}/S_{vv} = 0$$

$$S_{vh}/S_{vv} = 0$$



H:

$$S_{hh}/S_{vv} = +1$$

$$S_{hv}/S_{vv} = 0$$

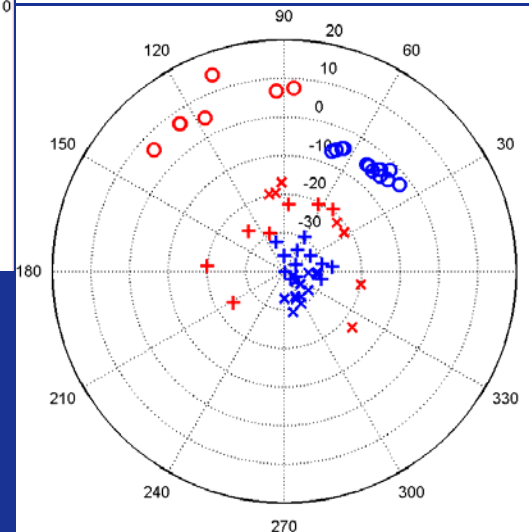
$$S_{vh}/S_{vv} = 0$$

D4:

$$S_{hh}/S_{vv} = -1$$

$$S_{hv}/S_{vv} = -1$$

$$S_{vh}/S_{vv} = -1$$



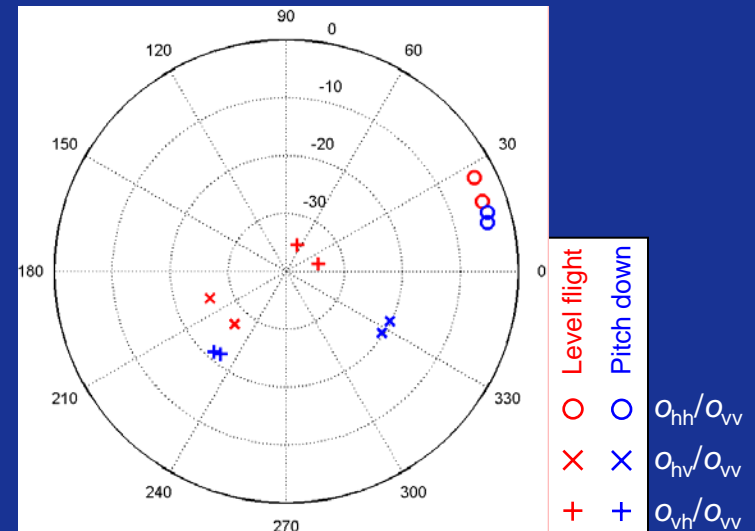
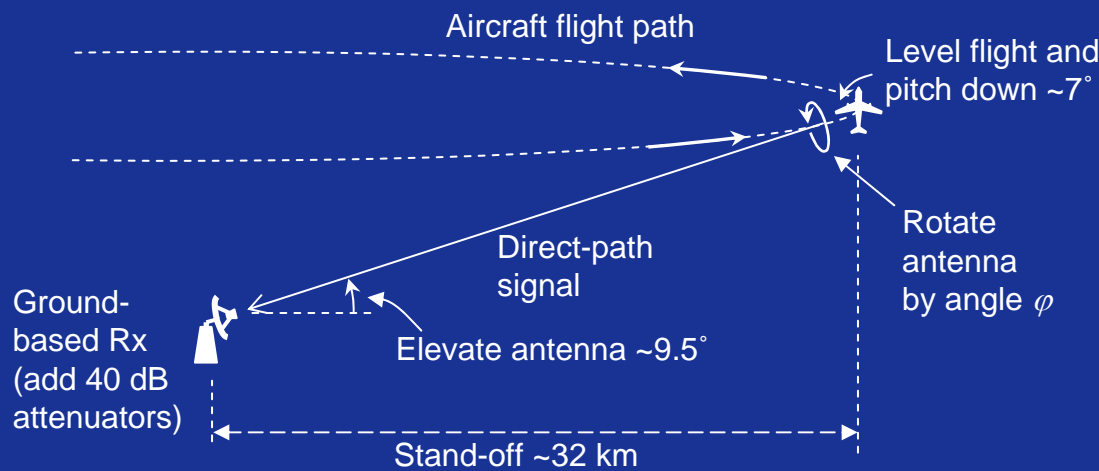


# Direct-path signal measurements

Direct-path signal measurements supplement the set of calibration target measurements.

'Scattering' matrix of direct-path signal is  $\mathbf{S} = \begin{bmatrix} -\cos \varphi & -\sin \varphi \\ -\sin \varphi & \cos \varphi \end{bmatrix}$

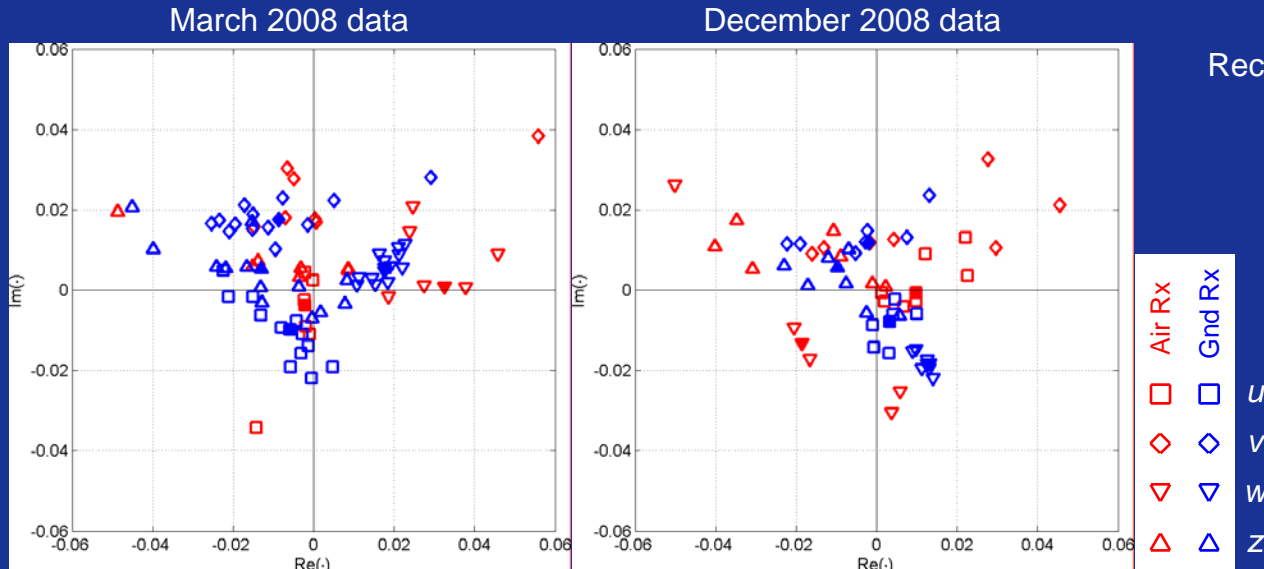
Estimate channel-imbalance from  $\begin{cases} \alpha = o_{vh}/o_{hv} \\ k = \pm j \sqrt{\frac{o_{hh}}{\alpha o_{vv}}} \end{cases}$  and/or  $k = \frac{o_{hh}}{o_{vh}} \tan \varphi = -\frac{o_{hv}}{o_{vv}} \cot \varphi$



December 2008 measurements



# Cross-talk estimation



Recall:  $\begin{cases} u = r_{vh}/r_{hh} & \leftarrow \text{Rx only} \\ v = t_{vh}/t_{vv} & \leftarrow \text{Tx only} \\ w = r_{hv}/r_{vv} & \leftarrow \text{Rx only} \\ z = t_{hv}/t_{hh} & \leftarrow \text{Tx only} \end{cases}$

Expect same  $v$  &  $z$  in air and ground data but different  $u$  &  $w$ .

For each run, initial cross-talk ratio  $u$ ,  $v$ ,  $w$ ,  $z$  estimates obtained using method Az.

Take 'median' of distributions to obtain final calibration parameters:

- $u^{(air)}$ : 'median' of  $u$  estimates from air data only
- $u^{(gnd)}$ : 'median' of  $u$  estimates from ground data only
- ◆  $v^{(air)}$ ,  $v^{(gnd)}$ : 'median' of pooled  $v$  estimates from air and ground data
- ▼  $w^{(air)}$ : 'median' of  $w$  estimates from air data only
- ▼  $w^{(gnd)}$ : 'median' of  $w$  estimates from ground data only
- ▲  $z^{(air)}$ ,  $z^{(gnd)}$ : 'median' of pooled  $z$  estimates from air and ground data

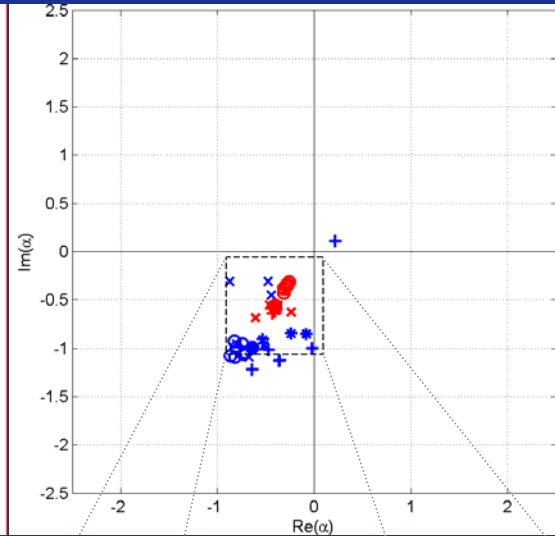
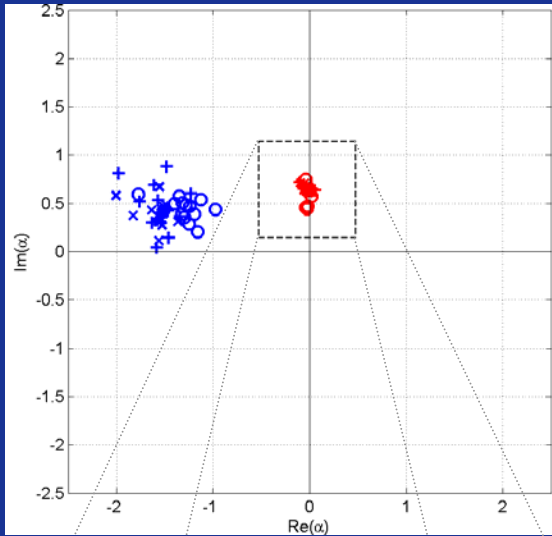
where 'median' of set of complex  $z_n$  is taken as:  $\text{median}(\{ \text{Re}(z_n) \mid n \}) + j \text{median}(\{ \text{Im}(z_n) \mid n \})$



# $\alpha$ estimation

March 2008 data

December 2008 data

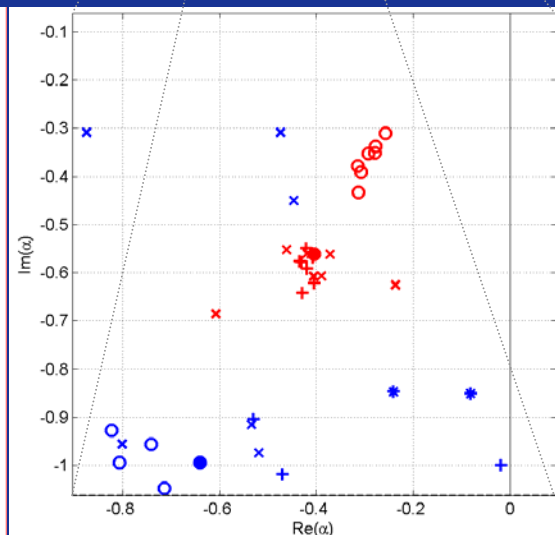
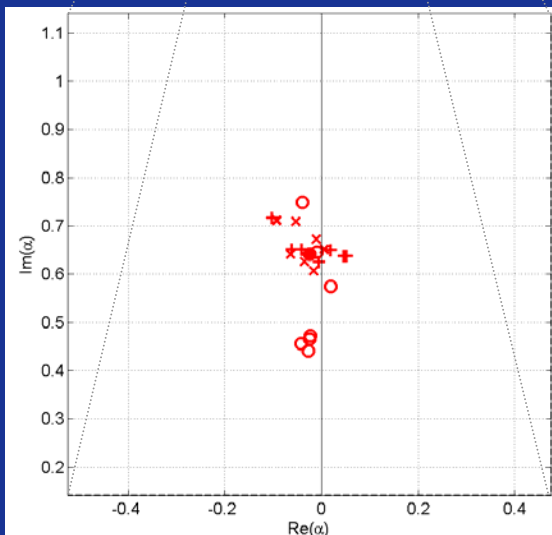


Initial  $\alpha$  estimates from individual runs

- Air Rx
- Ground Rx
- × D1
- × D1
- + D4
- + D4
- \* Direct-path

Final calibration solution:

- $\alpha^{(air)}$ : 'median' of air estimates
- $\alpha^{(gnd)}$ : 'median' of ground estimates

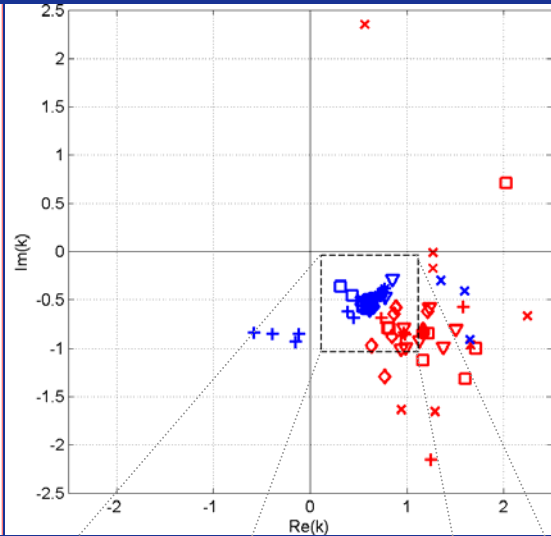
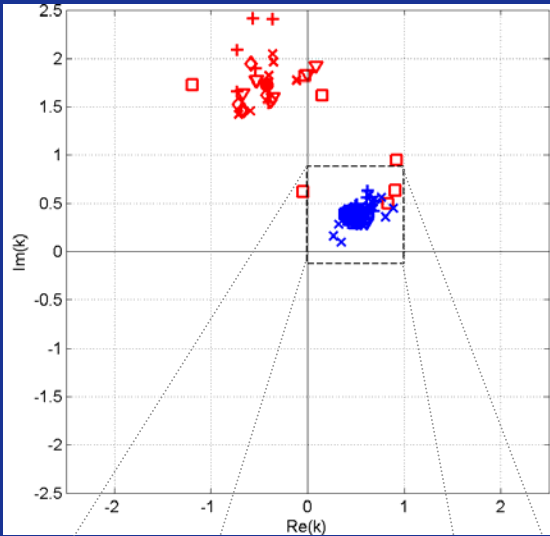




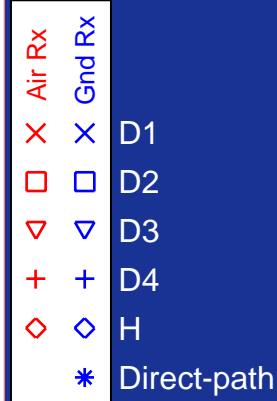
# $k$ estimation

March 2008 data

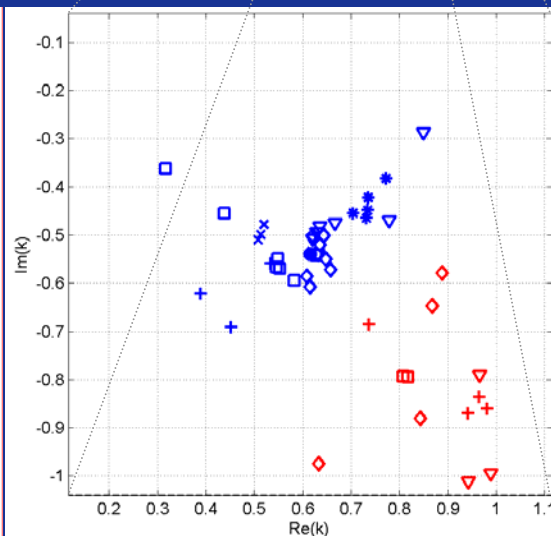
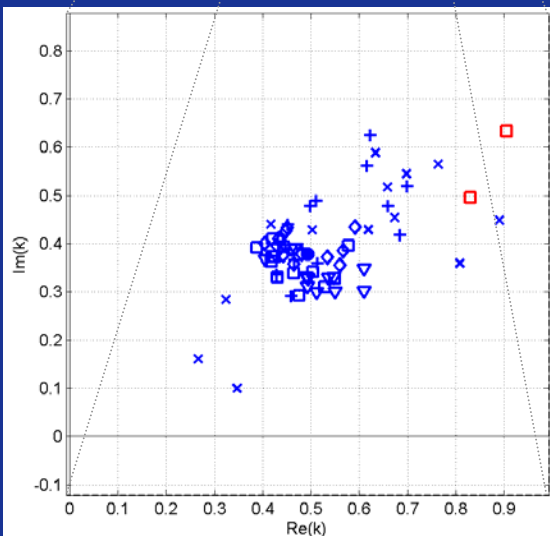
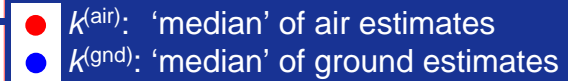
December 2008 data



Initial  $k$  estimates from individual runs

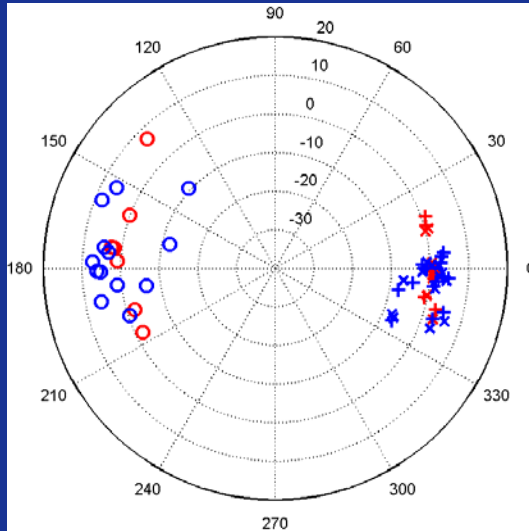


Final calibration solution:





# Post-calibration target measurements

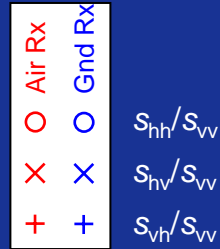


D1:

$$S_{hh}/S_{vv} = -1$$

$$S_{hv}/S_{vv} = +1$$

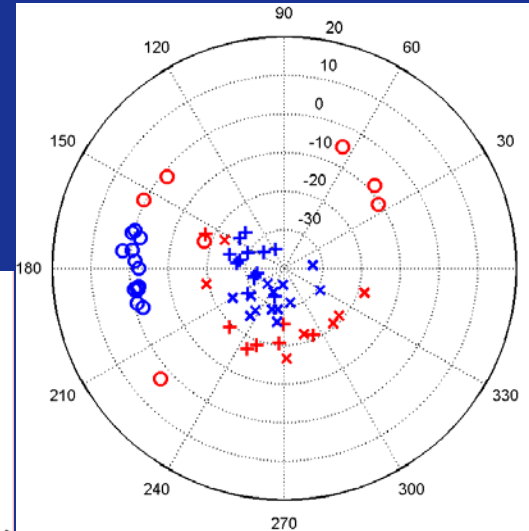
$$S_{vh}/S_{vv} = +1$$



$$S_{hh}/S_{vv}$$

$$S_{hv}/S_{vv}$$

$$S_{vh}/S_{vv}$$

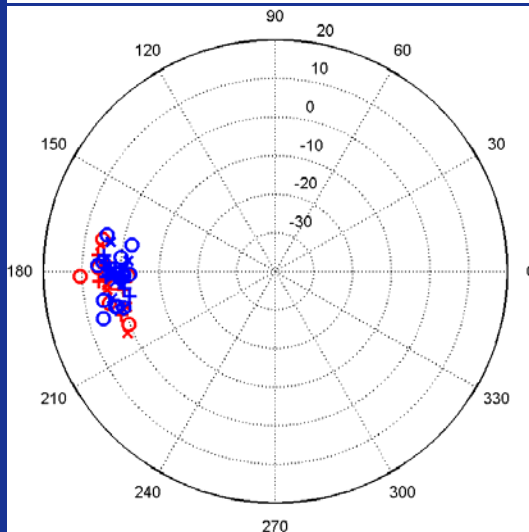


D2:

$$S_{hh}/S_{vv} = -1$$

$$S_{hv}/S_{vv} = 0$$

$$S_{vh}/S_{vv} = 0$$

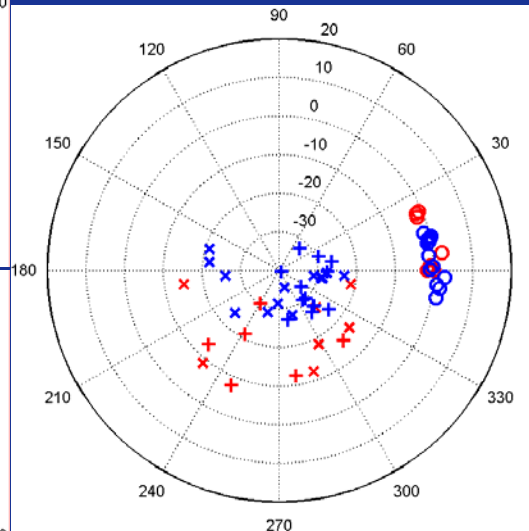


D3:

$$S_{hh}/S_{vv} = -1$$

$$S_{hv}/S_{vv} = 0$$

$$S_{vh}/S_{vv} = 0$$



H:

$$S_{hh}/S_{vv} = +1$$

$$S_{hv}/S_{vv} = 0$$

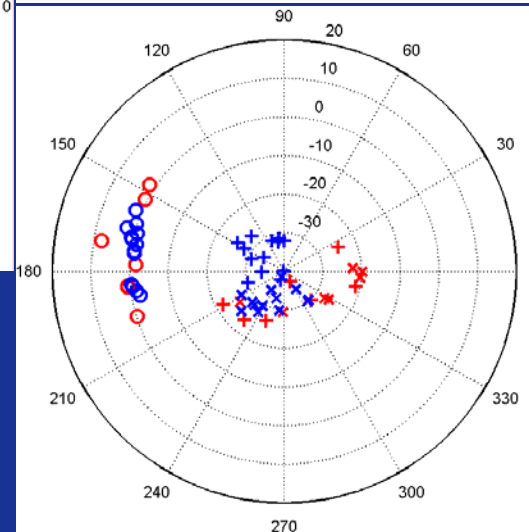
$$S_{vh}/S_{vv} = 0$$

D4:

$$S_{hh}/S_{vv} = -1$$

$$S_{hv}/S_{vv} = -1$$

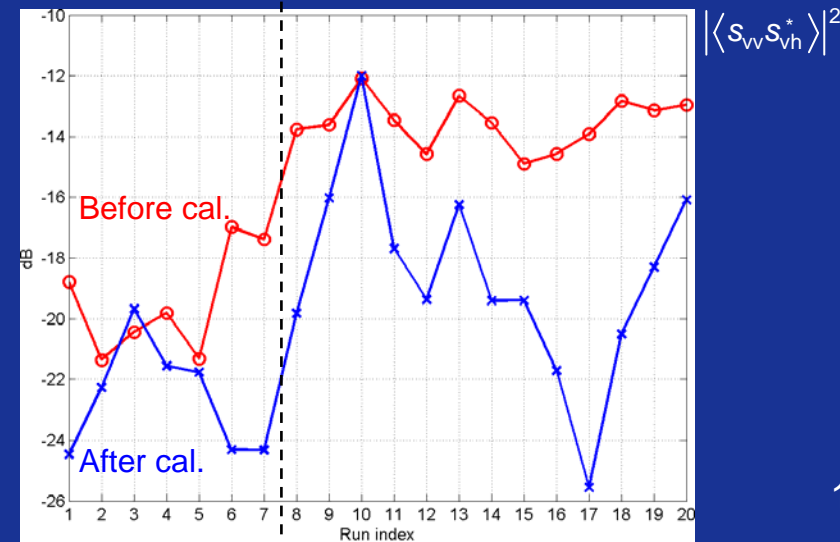
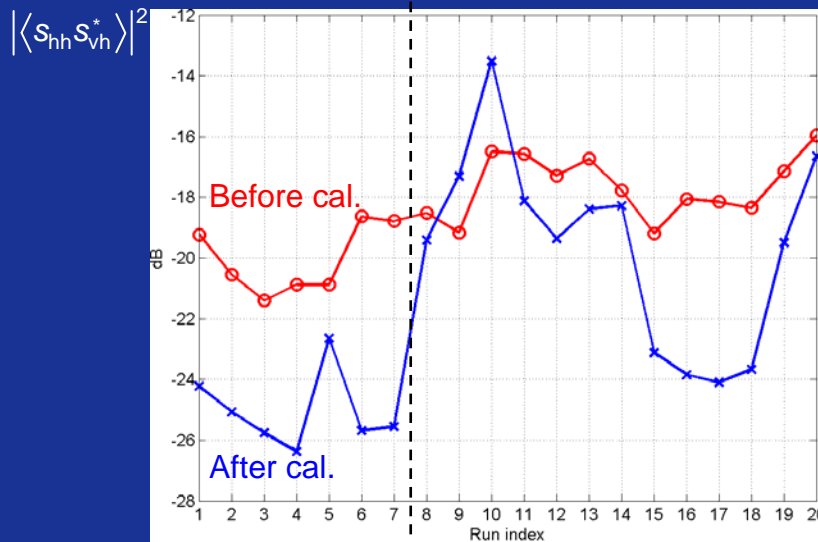
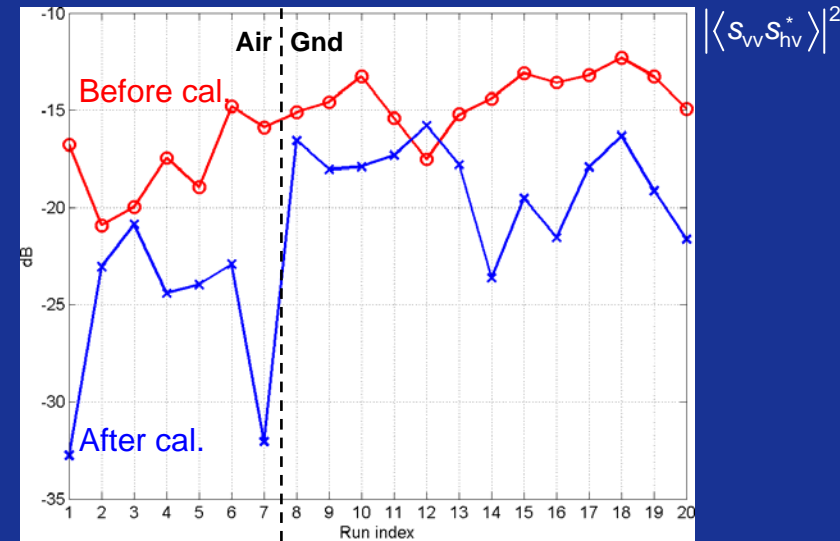
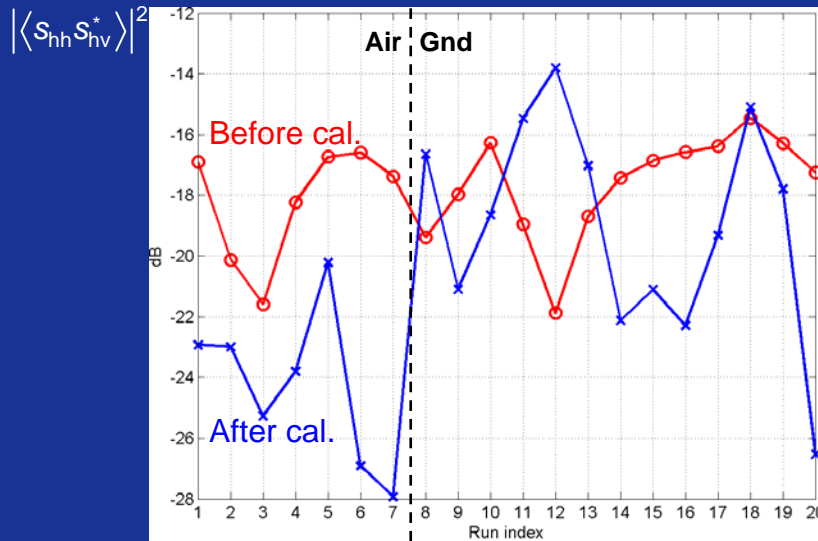
$$S_{vh}/S_{vv} = -1$$







# Distributed-target co-/cross-polar covariances



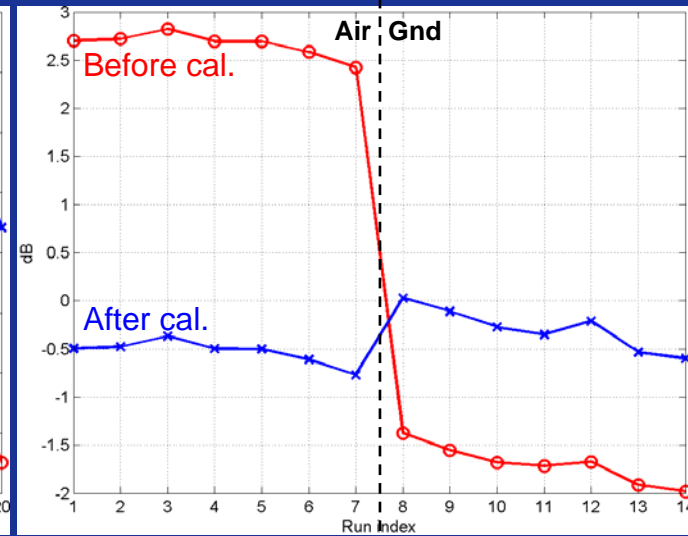
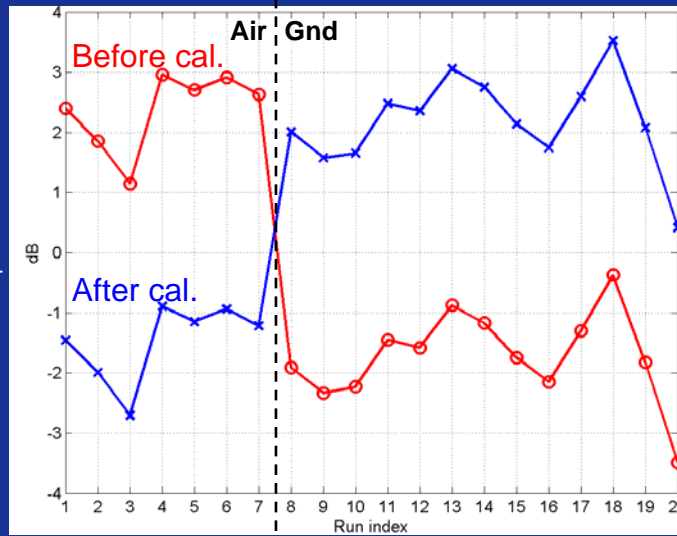


# Distributed-target cross-polar measurements

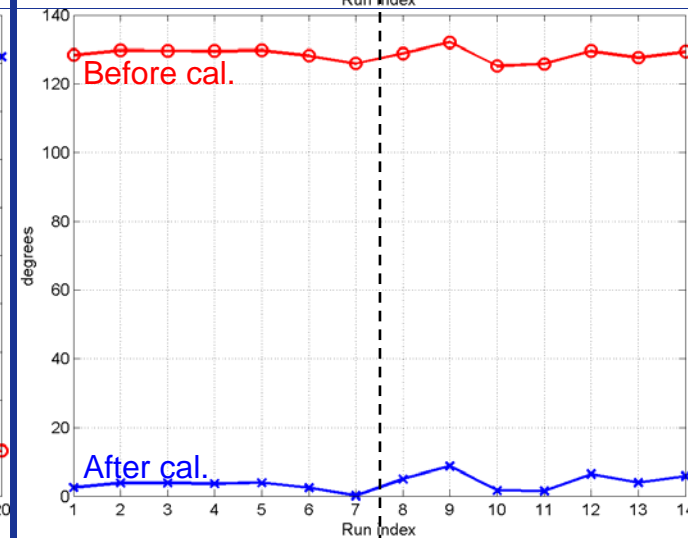
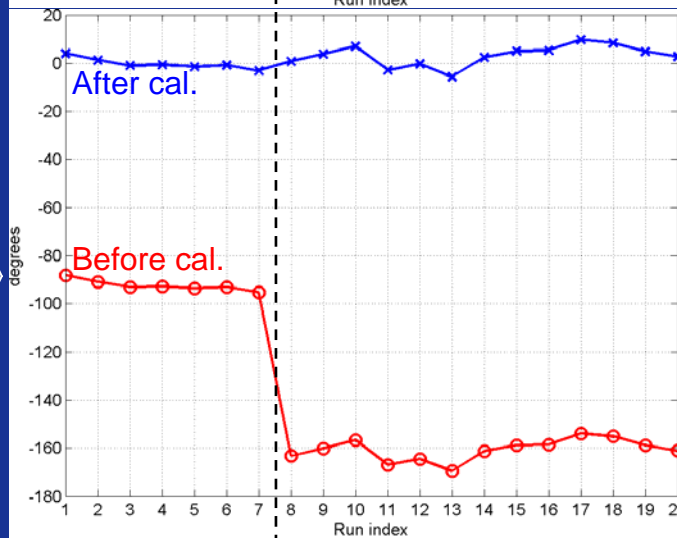
March 2008 data

December 2008 data

$$\frac{\langle |s_{hv}|^2 \rangle}{\langle |s_{vh}|^2 \rangle}$$



$$\angle \langle s_{hv} s_{vh}^* \rangle$$





# Conclusion

- A method for polarimetric calibration employing distributed-target, calibration-target and direct-path signal measurements has been applied to the *Ingara* monostatic and bistatic data.
- High variability is present in calibration target measurements possibly related to large range of look angles (e.g. bistatic from  $9^\circ$  to  $17^\circ$ ): use Polarimetric Active Radar Calibrators (PARCs) in future?
- Assumptions of distributed-target azimuthal-symmetry, i.e.  $\langle s_{ij} s_{ij}^* \rangle = 0$ , may not be valid: validity of cross-talk calibration solution is uncertain.
- Fair agreement in  $\alpha$  and  $k$  channel-imbalance estimates from distributed-target, calibration target and direct-path signal measurements is found.
- Application of calibration solution to measurements produces results generally more consistent with those expected of calibrated data.