

Target Design and Deployment for In-Field GeoSAR Calibration

Fugro-EarthData GeoSAR Technologies

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Regulatory Restrictions

- The UHF band is fully assigned to licensed users.
- GeoSAR must not cause interference to licensed users.
- On behalf of NGA, the NTIA coordinates GeoSAR access:
 - Provides list of licensed frequencies and bandwidth.
 - Communicates with local frequency coordinators to verify critical nointerference channels.
 - Provides GeoSAR with operational times.
- Old rules: must notch for transmitters within 20nmi of nadir, unless granted exemption.
- New rules: must notch if within "receiver" range of transmitter (300nmi!).





NOAA-1 P-band Transmit Waveform (Frequency Domain)







- Permanent calibration site in California.
- Use in notched environment? Calibrate in notched environment.
- Full UHF bandwidth is often available in tropical areas.
- Options:
 - Find a site in the continental US where we aren't required to notch.
 - Find a site overseas where we aren't required to notch.
 - Calculate the effects of notching and compensate for them when notching changes significantly.
- Interferometric calibration
 - requires an accurate, predominantly flat DEM.
- Radiometric (and polarimetric) calibration
 - can be done *in-field* if we have targets available.



Rationale for In-field Radiometric Calibration

- System changes don't require return to permanent calibration site.
- Possible to monitor radiometric calibration solution to determine system stability.
- On mapping campaigns we deploy reference targets anyway.
- Contemporaneous calibration solution.







- Small and "easily" deployed.
- Current design consists of a tripod base and a set of three, interlocking plates.
- ~30dBm² pk RCS.









P-band Targets

- Large: 2.2m internal face side length. Heavy: ~100lbs
- Simple construction: in-country fabrication templates ensure regularization.
- Placement strategy! Optimal locations not always available.







- Flight plan.
- Site identification.
- Surveyor choice.
- Site survey, base and rover GPS setup. Base run for +-15 mins around rover acquisition. Survey nail marks reflector location.
- Field location recorded and communicated.
- Target alignment calculated based on flight path, and field location.
- Targets constructed and deployed.
- Target phase centre recorded
- Targets secured.





Successful Deployment Example: Peru

- Example of target deployment.
- Crated targets to Lima.
- Trucked to survey site.
- Erected at site and GPS locations provided.
- Target alignments calculated and communicated to fieldteam.
- Targets aligned and imaged.
- Focused targets appear in the imagery and can be used for radiometric calibration ...



Successful Deployment Example: Peru





Target site some 370 miles from Lima as the Condor flies ...

www.fugro.com



Deployment Example: Peru



... over 3000m above sea level. Images are SLC.

www.fugro.com

P-band Target RCS Calculation



software for electromagnetic design

P-band Target RCS Calculation



software for electromagnetic design



Use of Target RCS in Calibration

- Planned process:
 - MoM full complex scattering matrix calculations.
 - Waypoints on the *flown* flight path + knowledge of target location and orientation.
 - Antenna pattern, orientation, gain, range info. yield scattering amplitudes.
 - Antenna frame HH,HV response of the target recovered from the scattering matrix by basis rotation about LOS.
 - The along-track target responses can be integrated.
 - Several targets can be used to yield a calibration constant.
 - Approach mirrors that used by ONERA (Laurette Pastore, PhD Thesis, *Imagerie Radar par Synthese d'Ouverture en Basse Frequence*, 2002)
 - Frequency dependence of target response can be used to understand range response.



P-band



X-band



Depolarizing Trihedrals



 $\hat{\mathbf{k}}_i = -\sin\theta\cos\phi\,\hat{\mathbf{x}} - \sin\theta\sin\phi\,\hat{\mathbf{y}} - \cos\theta\,\hat{\mathbf{z}}$

- High-frequency model.
- For a traditional (PEC) corner reflector we would have

$$R_{v3} = 1$$

and

$$R_{_{h3}} = -1$$

• and the cross-polar scattering amplitude would be zero.

$$S_{hh} = \gamma_{i3}^2 \gamma_{i2}^2 \left[1 - \sin^2 \theta \sin^2 \phi \right] \left(R_{h3} \cos^2 \theta \cos^2 \phi - R_{v3} \sin^2 \phi \right)$$
$$S_{vh} = \left(R_{v3} + R_{h3} \right) \gamma_{i3}^2 \gamma_{i2}^2 \left[1 - \sin^2 \theta \sin^2 \phi \right] \cos \theta \sin \phi \cos \phi$$



Depolarizing Trihedrals



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The Gridded Trihedral: A New Polarimetric SAR Calibration Reflector, D R Sheen, et al, IEEE TGRS, Nov, 1992.



$$\hat{\mathbf{k}}_i = -\sin\theta\cos\phi\,\hat{\mathbf{x}} - \sin\theta\sin\phi\,\hat{\mathbf{y}} - \cos\theta\,\hat{\mathbf{z}}$$

$$S_{hh} = \gamma_{i3}^2 \gamma_{i2}^2 \left[1 - \sin^2 \theta \sin^2 \phi \right] \left(R_{h3} \cos^2 \theta \cos^2 \phi - R_{v3} \sin^2 \phi \right)$$

 $S_{vh} = (R_{v3} + R_{h3}) \gamma_{i3}^2 \gamma_{i2}^2 [1 - \sin^2 \theta \sin^2 \phi] \cos \theta \sin \phi \cos \phi$

• Replace a reflecting surface with a waveguide that reflects one polarization preferentially and S_{hv} is no longer zero ...

$$\hat{\mathbf{h}}_{i3} = \gamma_{i3} \left(-\cos\theta \,\hat{\mathbf{y}} + \sin\theta\sin\phi \,\hat{\mathbf{z}} \right)$$
$$\gamma_{i3} = \left[\cos^2\theta + \sin^2\theta \sin^2\phi \right]^{-1/2}$$

P-band Depolarizing Trihedral





• Prototype P-band depolarizing corner reflector in hangar.

P-band Depolarizing Corner RCS Calculation



P-band Depolarizing Corner RCS Calculation





Summary



- Notching requirements at UHF imply a need to calibrate outside the USA.
- We have designed new targets for radiometric and polarimetric calibration and are investigating their responses (GeoSAR quad-pol upgrade is in progress).
- We have designed a process for deployment of targets during campaigns and tested the process in an overseas deployment.
- We will continue to improve the *in-field* calibration process by incorporating the target scattering pattern and flight path information.
- Thank you!



X-band and P-band targets visible in the X-band image